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(54) **HEAT RELEASE RATE CALORIMETER FOR MILLIGRAM SAMPLES**

JP 3009861 * 1/1988 436/157

OTHER PUBLICATIONS

(75) Inventor: **Richard E. Lyon**, Absecon, NJ (US)
(73) Assignee: **The United States of America as represented by the Secretary of Transportation**, Washington, DC (US)
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Microscale Combustion Calorimeter DOT/FAA/AR-01/117 Final Report Feb. 2002.
Lyon, Solid-State Thermochemistry of Flaming Combustion, appearing as Chapter 11 in *Fire Retardancy of Polymeric Materials*, edited by Grand, et al.; Marcel Dekker, Inc., 2000.
Reshetnikov, et al., Oxidation kinetic of volatile polymer degradation products, *Polymer Degradation and Stability* 64 (1999).
Gracik, et al., A novel thermogravimetric technique for determining flammability characteristics of polymeric materials, *Thermochimica Acta*, 212 (1992).

(List continued on next page.)

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Primary Examiner—Diego Gutierrez
Assistant Examiner—Gail Verbitsky
(74) *Attorney, Agent, or Firm*—James J. Drew; Otto M. Wildensteiner

(56) **References Cited**

U.S. PATENT DOCUMENTS

2,458,610 A * 1/1949 Lindstrom 436/160
3,096,157 A * 7/1963 Brown et al. 436/160
3,853,474 A * 12/1974 Austin 436/160
3,933,429 A * 1/1976 Shibata et al. 436/160
4,229,967 A * 10/1980 Kneifel et al. 73/15 R
4,499,191 A * 2/1985 Bruning et al. 436/160
4,761,078 A 8/1988 Farris et al.
5,235,862 A * 8/1993 Harada 436/157
5,981,290 A 11/1999 Lyon et al.
6,312,154 B1 * 11/2001 Schick et al. 374/36
6,371,147 B1 * 4/2002 Philippe 137/6
2001/0018218 A1 * 8/2001 Ragaglia et al. 436/160

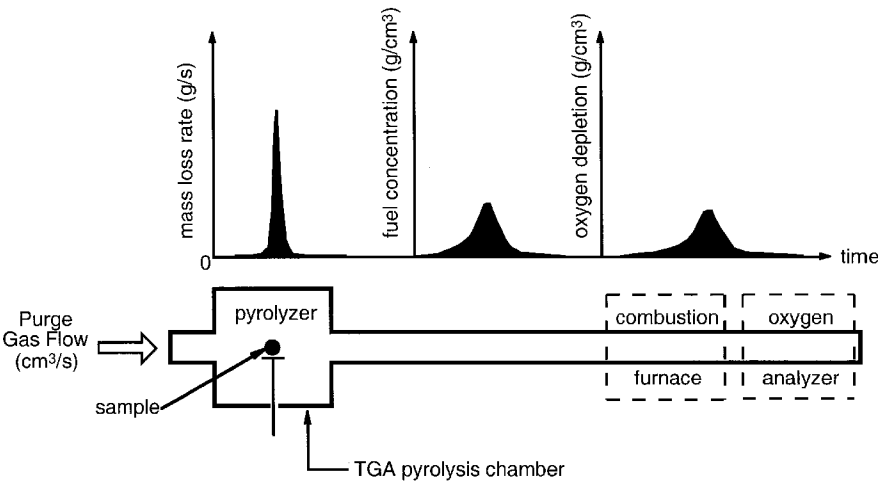
FOREIGN PATENT DOCUMENTS

JP 0173466 * 9/1985 436/160

ABSTRACT

A calorimeter that measures heat release rates of very small samples (on the order of one to 10 milligrams) without the need to separately and simultaneously measure the mass loss rate of the sample and the heat of combustion of the fuel gases produced during the fuel generation process. The sample is thermally decomposed in a small volume pyrolysis chamber. The resulting fuel gases are immediately swept by an inert gas stream from the pyrolysis chamber into a combustion furnace in a plug-like flow. This plug flow substantially synchronizes the emerging fuel gases with the mass loss rate of the sample. Oxygen is metered into the fuel gas stream just before it enters the combustion furnace where the fuel gases are completely oxidized. The effluent from the furnace is analyzed to determine the amount of oxygen consumed per unit time and the heat release rate is computed without the need to separately measure the mass loss rate of the sample.

6 Claims, 3 Drawing Sheets



OTHER PUBLICATIONS

Parker, Determination of the Input Data for a Model of the Heat Release Rate of Wood, *Special Technical Publication* 983 (1988), American Society for Testing and Materials.

Susot, Characterization of the Thermal Properties of Forest Fuels by Combustible Gas Analysis, *Forest Science*. vol. 28, No. 2 (1982), Society of American Foresters.

Susot, et al., A Quantitative Thermal Analysis Technique for Combustible Gas Detection, *Journal of Fire & Flammability*, vol. 10 (Apr. 1979).

Lyon, et al., A Pyrolysis-Combustion Flow Calorimeter Study of Polymer Heat Release Rate, a paper presented at the Ninth Annual BCC Conference on Flame Retardancy, Jun. 1998.

Kifer, et al., Thermal Evolution Analysis of Some Organic Materials, *Analytic Calorimetry*, 1974.

* cited by examiner

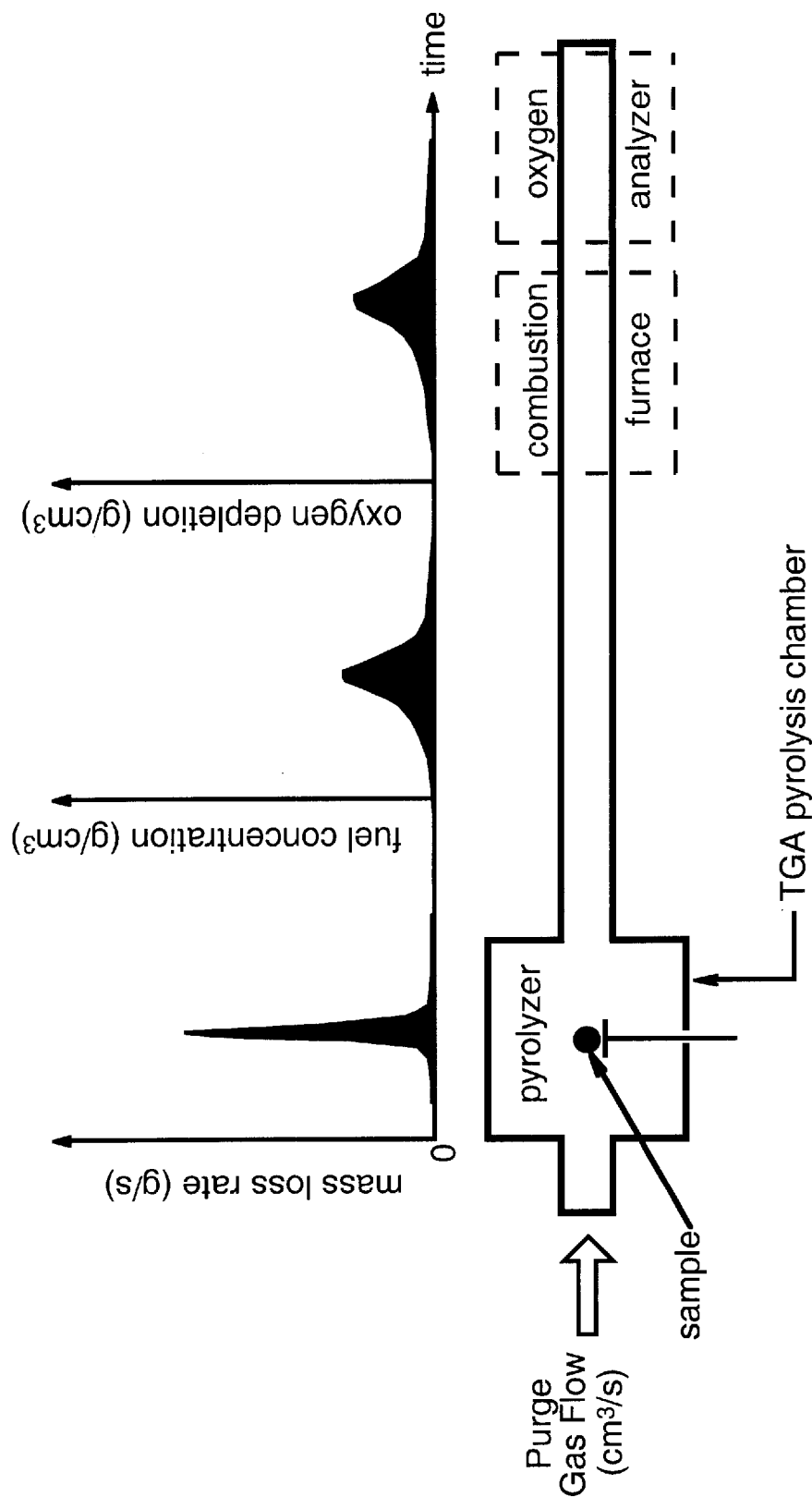


Figure 1

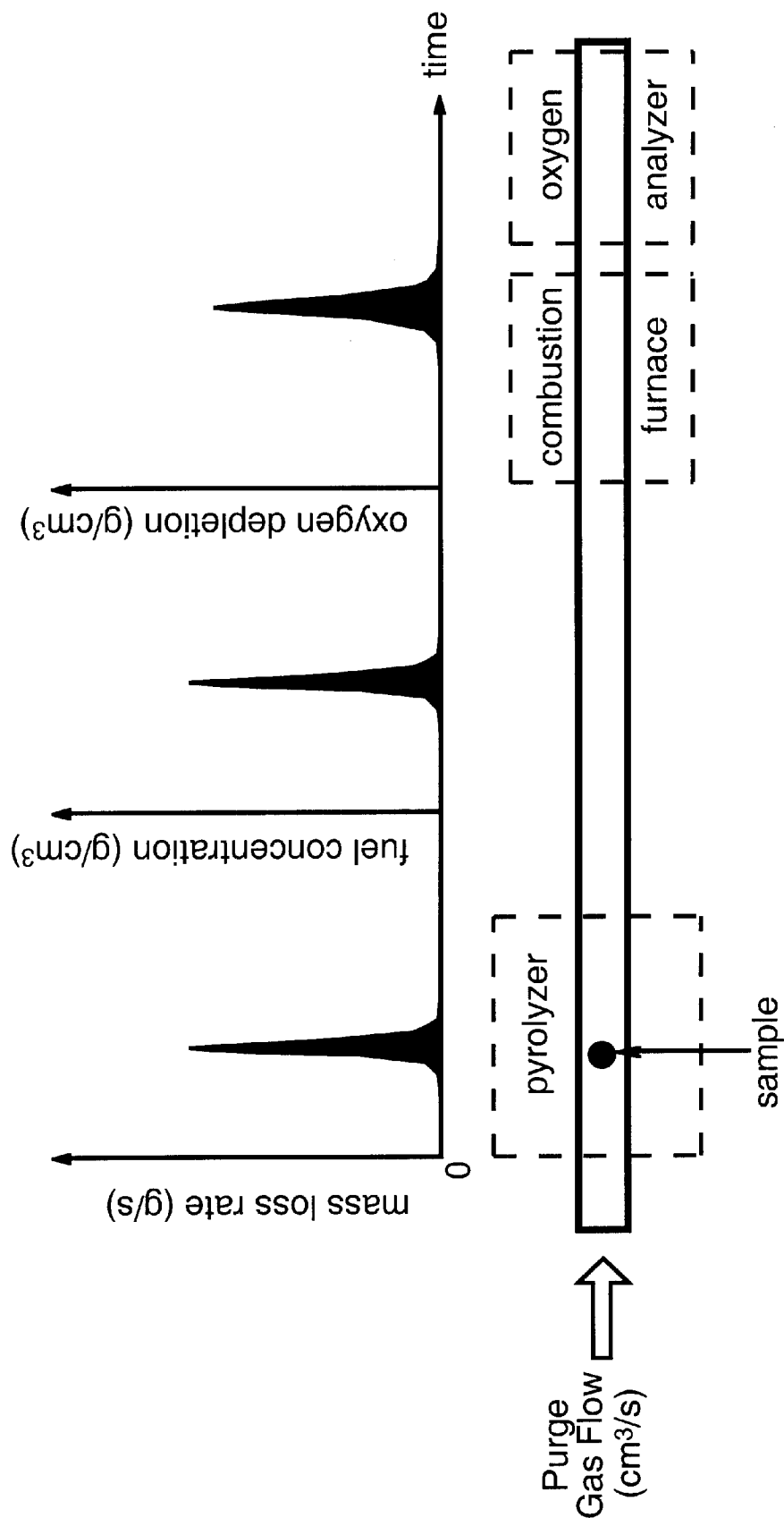


Figure 2

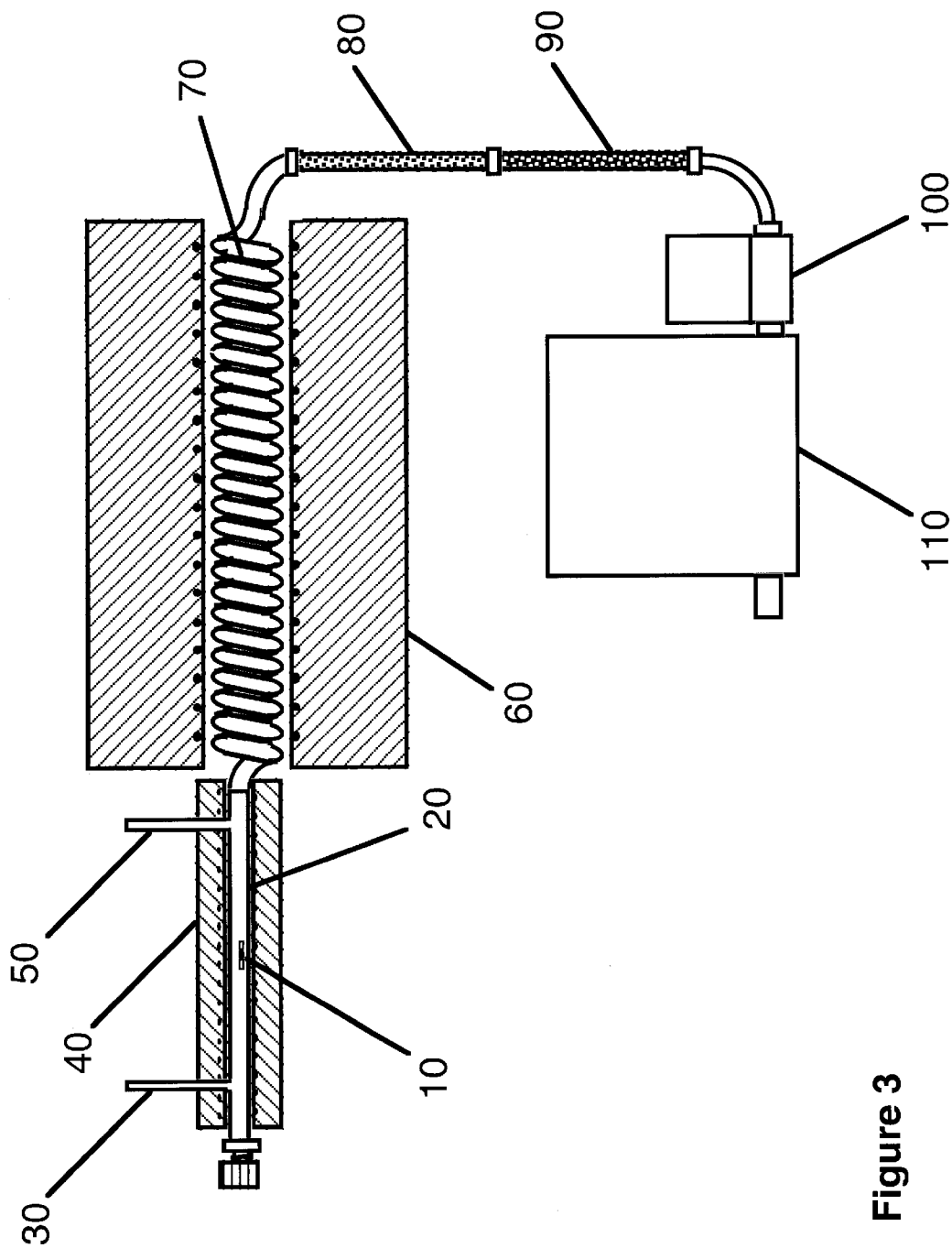


Figure 3

HEAT RELEASE RATE CALORIMETER FOR
MILLIGRAM SAMPLES

The invention described herein may be manufactured,
used, and licensed by or for the Government of the United
States without the payment to me of any royalties thereon.

FIELD OF THE INVENTION

The present invention relates generally to calorimeters,
and more particularly to calorimeters used to measure heat
release rates of small samples. Such calorimeters are useful
in determining flammability parameters of milligram
samples of combustible materials.

BACKGROUND OF THE INVENTION

The rate at which heat is released during the burning of a
combustible solid in a fire is the primary indicator of its
hazard to life and property. Consequently, a method to study
the heat release rate of solids in a fire or under fire conditions
is of theoretical and practical importance to fire protection
engineers and materials scientists. Fire calorimeters are used
to measure the rate of heat released in flaming combustion,
often with simultaneous measurement of the fuel generation
(mass loss) rate of the solid. Since the combustion reactions
in the flame are orders of magnitude faster than the fuel
generation rate of the solid and the transit time of the
gaseous fuel between the burning surface and the flame
where combustion occurs is less than one second, the slow
step (that is, the step limiting the burning rate in flaming
combustion of solids) is the fuel generation rate. This means
that the heat released in flaming combustion is essentially
simultaneous with, and proportional to, the mass loss of the
solid, and that the heat release rate in a fire is simultaneous
with, and proportional to, the mass loss rate at the surface of
the material.

Fire calorimeters measure the heat release rate in flaming
combustion directly but have drawbacks for materials
research or quality control testing. These drawbacks include:
1) the heating rate in the sample varies with location; 2) the
temperature of the sample is non-uniform because of thick-
ness and edge effects; 3) the amount of oxygen diffusing into
the flame is usually less than is required to effect complete
combustion of the fuel gases, so that measured heat release
rate depends on the test environment; 4) the measured heat
release rate depends on the sample thickness, orientation,
and method of holding the sample, (i.e., on the test method);
5) fire calorimeters give qualitative (about 15% error) rather
than quantitative (about 5% error, or less) heat release rate
data because of the poor repeatability of the test as a result
of drawbacks 1) through 4) above; 6) samples must be large
(on the order of about 100 grams) to support steady flaming
combustion; and 7) replicate samples are needed because of
the poor repeatability of fire calorimetry tests. Thermo-
formed kilogram samples are impractical for research where
initial synthesis of new materials typically yields one (1)
gram of material. Gram quantities of sample can be used for
ease of ignition (flammability) tests utilizing a Bunsen
burner but only pass/fail results are obtainable and repro-
ducibility is poor.

Because flaming combustion requires large samples and
the thermal history and combustion environment vary from
sample to sample, fire calorimetry is not the method of
choice for measuring the fire performance properties of
materials. Likewise, ignitability tests provide only relative
rankings but no properties that can be related to fire perfor-
mance. A number of thermoanalytical methods have been

developed which use thermal decomposition of milligram-
sized samples and analysis of the evolved gases to measure
the heat released under controlled (laboratory) conditions.
Of those known laboratory thermoanalytical methods which
have been used to measure the non-flaming heat of com-
bustion of the sample gases under simulated fire conditions,
all measure the total heat of combustion of the sample
pyrolysis (fuel) gases. However, only the methods that
measure the mass loss rate of the sample can determine heat
release rate of an individual material particle (specific heat
release rate) as it occurs at a burning surface in a fire. The
heat release rate in a fire during steady flaming combustion
is equal to the specific mass loss rate (rate at which the solid
particle decomposes into fuel which can enter the gas
phase/flame) multiplied by the thickness of the surface
burning layer (number of solid particles involved), the heat
of combustion of the particles (heat released per particle by
complete combustion), and the efficiency of the combustion
process in the flame (fraction of solid particles which enter
the gas phase and are completely combusted). Because the
rate of mass loss at the burning surface is a relatively slow
process in comparison to the gas phase combustion
reactions, the heat release in a fire is coincident in time with,
and proportional to, the mass loss (fuel generation) rate of
the sample. Consequently, unless the evolved gas measure-
ment is synchronized with the sample mass loss in a labo-
ratory test, the heat release rate as it occurs in a fire cannot
be measured. One approach to obtain the rate of heat
released by the sample under fire conditions is to measure
mass loss (fuel generation) rate and heat of combustion of
the fuel gases separately and then multiply them together.

Lyon and Walters have invented and patented a micros-
cale combustion calorimeter that measures flammability
parameters of milligram samples of combustible materials.
U.S. Pat. No. 5,981,290. In order to obtain results consistent
with other techniques, the invention requires the simulta-
neous measurements of the mass loss rate of the sample, and
the amount of oxygen consumed by combustion of the fuel
gases given off by the sample. The mass loss rate is
measured by using a thermogravimetric analyzer (TGA),
while the amount of oxygen consumed is measured using a
mass flow meter and oxygen analyzer downstream from the
combustor.

Errors of more than 50% result when the heat release rate
of the sample is determined solely from the oxygen con-
sumption rate without a mass loss rate measurement. These
errors arise principally from two sources: (1) distortion of
the heat release rate curve and (2) reduced area under the
heat release rate curve. Each of these sources of error will be
discussed in turn.

**DISTORTION OF THE HEAT RELEASE RATE
CURVE:** The mass loss (fuel generation) event for a rapidly
heated small sample of combustible material occurs over a
narrow time interval. The mass loss/fuel generation rate
versus time curve has the form of a narrow peak or "fuel
pulse". Multiple fuel pulses are observed for multi-
component materials. The shape of the fuel pulse is unique
to a particular material or component. This fuel pulse
becomes spread out, broadened, or "smeared" if it is gen-
erated in a large volume (e.g., the pyrolysis chambers of
commercial thermogravimetric analyzers) where the fuel
gases can be intermingled, mixed, and diluted with the purge
gas before exiting to the combustion chamber or furnace.
This same intermingling, mixing, and dilution occurs any-
where in the flow calorimeter where a large volume is
introduced (e.g., the scrubbers). The large volume of the
TGA has the effect of distorting the shape of the fuel pulse

prior to its reaction with oxygen in the combustor or furnace. Large volumes further downstream distort the shape of the combustion gases before the oxygen content of the combustion products can be measured. Consequently, the oxygen consumption history measured at the downstream oxygen detector has been distorted by the instrument and is not synchronized with the fuel pulse of the material. In particular, instrumental broadening or smearing reduces the height and increases the width (duration) of the fuel pulse as deduced from oxygen consumption.

Of particular interest to fire scientists is the peak specific heat release rate of the sample (W/g). The peak specific heat release rate of a material is a quantitative measure of its fire hazard and is obtained by multiplying the height of the fuel pulse (maximum fuel generation rate, g/g-s) by the instantaneous heat of combustion of the fuel (J/g) at peak mass loss rate. The average heat of combustion of the fuel is proportional to the area under the oxygen consumption curve and is unaffected by instrumental broadening of the fuel pulse. The instantaneous heat of combustion of the fuel gases given off at peak mass loss rate cannot be determined, however, unless the oxygen consumption rate and mass loss rate are synchronized.

In the Lyon and Walters patent cited, the TGA is a Perkin-Elmer TGA System 7 with a pyrolysis chamber volume of approximately $V=50$ cubic centimeters (50 cm^3) which is typical of commercial TGA's. The residence time of the pyrolysis gases in the pyrolysis chamber is V/F where F is the volumetric flowrate of the purge gas entering the pyrolysis chamber. In the invention as practiced by Lyon and Walters $F=100\text{ cm}^3$ per minute and $V=50\text{ cm}^3$ so the residence time of the fuel gases in the pyrolysis chamber is $V/F=(50\text{ cm}^3)/(100\text{ cm}^3/\text{min})=0.5\text{ minutes}=30\text{ seconds}$. During this residence time of 30 seconds in the pyrolysis chamber pyrolysis products are continuously intermingled, mixed, and diluted with the entering purge gas (typically nitrogen) before exiting to the combustor, flow meter and oxygen analyzer. Errors arise because this residence time in the pyrolysis chamber is long compared to the time interval Δt over which the fuel gases are generated during the heating program, i.e., the fuel pulse width. The fuel pulse width is related to the temperature range over which the sample decomposes ΔT and the heating rate R as $\Delta t=\Delta T/R$. In the invention practiced by Lyon and Walters the typical heating rate is $R=100\text{ K/min}$ and the typical pyrolysis temperature interval is $\Delta T=50\text{ K}$, so that the time interval over which fuel gases are produced (i.e., the fuel pulse width) is $\Delta t=\Delta T/R=(50\text{ K})/(100\text{ K/min})=0.5\text{ minutes}=30\text{ seconds}$. The long residence time of the fuel gases in the pyrolysis chamber (30 seconds) relative to the fuel pulse width (15 seconds) results in the fuel gases being intermingled, mixed, and diluted with the purge gas before exiting. These effects distort (smear) the fuel pulse and the associated oxygen consumption history. Thus, for typical TGA pyrolysis chambers the fuel generation (mass loss) history is not coincident with, and proportional to, the oxygen consumption history, so the oxygen consumption history cannot be used to determine the heat release rate of the sample as occurs in the pyrolysis chamber or in a fire.

REDUCED AREA UNDER THE HEAT RELEASE RATE CURVE: High molecular weight organic compounds (tars) are fuels of low volatility (high boiling temperature) produced during polymer thermal decomposition. In fires where surface temperatures are high (ranging from about 400°C . to about 800°C .) these tars are gaseous and contribute substantially to the heat release rate in flaming combustion. In commercial thermogravimetric analyzers the

pyrolysis chamber wall temperature is substantially lower than the boiling temperature of these tars. As a result, the tar tends to condense on the pyrolysis chamber wall as a liquid and is not transported in the gas stream which enters the combustor for reaction with oxygen. This results in less oxygen consumption and low apparent total heat release values (area under the heat release rate versus time curve).

For the foregoing reasons, there is a need for a calorimeter that can more accurately measure the heat release rate of milligram samples of materials.

OBJECTS OF THE INVENTION

Accordingly, it is an object of the present invention to provide a means and method for accurately measuring flammability parameters of milligram samples of combustible materials.

It is a further object of the present invention to provide a means and method for accurately measuring the heat release rates of milligram samples of combustible materials without the need to simultaneously measure the mass loss rate of the sample and the heat of combustion of the fuel gases.

It is a further object of the present invention to provide a means and method for measuring the heat release rate of milligram samples of combustible materials using a flow calorimeter with minimal distortion of the fuel gas profile produced by the pyrolyzation of the sample.

It is a still further object of the present invention to provide a means and method for measuring the heat release rate of milligram samples of combustible materials using a flow calorimeter and a simple analytical relationship applied to measured oxygen gas consumption.

It is a still further object of the present invention to provide a means and method for measuring the heat release rate of milligram samples of combustible materials using a flow calorimeter in which all the products of pyrolysis are captured and analyzed.

SUMMARY

Briefly, the present invention is a calorimeter that measures heat release rates of very small samples (on the order of one to 10 milligrams) without the need to separately and simultaneously measure the mass loss rate of the sample and the heat of combustion of the fuel gases produced during the mass loss process. This is accomplished by minimizing the size of the pyrolysis chamber so that the fuel gases are not intermingled nor diluted by the purge gas but instead travel through the instrument as a small plug of fuel gases. Eliminating the TGA, with its relatively large volume, reduces the pyrolysis volume, and thereby eliminates the need for the TGA in the first place. Eliminating the TGA has at least two advantages. First, it prevents the condensation of tars produced in the pyrolysis chamber and permits these high molecular weight fuels to contribute to the total combustion of the pyrolysis products. Second, this minimal intermingling of the fuel gases and dilution by the purge gas, enhances "plug flow" through the instrument, effectively synchronizing the oxygen consumption history with the sample mass loss history. Such synchronization permits a simple mathematical relation between the two quantities and the desired heat release rate of the sample.

BRIEF DESCRIPTION OF THE DRAWING

FIG. 1 is an idealized representation of an earlier calorimeter illustrating the fuel generation rate (mass loss rate) profile, the fuel concentration profile prior to entering the

combustion chamber, or furnace, and the oxygen depletion profile of the gases emerging from the furnace.

FIG. 2 is an idealized representation of one embodiment of the invention illustrating the fuel generation rate (mass loss rate) profile, the fuel concentration profile prior to entering the combustion chamber (or furnace), and the oxygen depletion profile of the gases emerging from the furnace.

FIG. 3 is a schematic representation of one embodiment of the invention.

DETAILED DESCRIPTION

In FIG. 1, a sample is pyrolyzed in a conventional thermogravimetric analyzer; the fuel gases produced by the pyrolysis are carried through a narrow tube by an inert purge gas toward a combustion chamber; a constant flow of oxygen sufficient to completely oxidize the fuel gases is metered into the gas stream, and then the fuel gases, the purge gas, and the oxygen are conducted into a combustion chamber where the fuel gases are completely oxidized. The oxygen depletion is measured over time to determine the rate at which fuel was generated by the pyrolysis of the sample. Because the oxygen depletion profile is "smeared" with respect to the fuel concentration profile, the simultaneous measurement of the mass loss rate of the sample is needed to accurately measure the fuel generation rate using this approach.

In FIG. 2, the TGA, with its associated large volume, has been removed. Immediately, the problem of tar condensation on the walls of the TGA is eliminated. All of the fuel gases are then carried, synchronized with the sample mass loss rate, within the tube in a "plug-like" flow with greatly reduced intermingling, mixing, and dilution with the purge gas. Oxygen is metered into the plug as it enters the combustion chamber. The oxygen depletion profile mimics the fuel concentration profile, and also, the mass loss rate profile. The strong similarity of the oxygen depletion profile to the fuel concentration profile suggests that the events are synchronized and, consequently, the need to separately measure the mass loss rate is eliminated.

In FIG. 3, sample 10 is thermally decomposed (pyrolyzed) in small diameter pyrolysis tube 20 through which flows an inert purge gas (e.g., N₂) introduced through purge gas inlet tube 30. Typically, pyrolysis tube 20 is a quarter-inch (outer diameter) Inconel™ or similar tube about 6 inches long. Pyrolysis tube 20 runs through an electrical heater that raises the temperature of the sample. In this embodiment, the temperature increase is monotonic, but that is not necessary. As sample 10 is thermally decomposing, it produces fuel gases (products of decomposition), that are oxidized by mixing with a measured amount of oxygen or air introduced through oxidizer gas inlet 50. Oxidation takes place in combustion tube coil 70 that has an extended length of more than 12 inches, typically, 16 feet. Combustion tube coil 70 can also be fabricated from quarter-inch Inconel™ or similar tubing that is heat and chemical resistant. Combustion tube coil 70 is enclosed in insulated combustion furnace 60 where the fuel gases and oxidizer are heated to high temperature to convert the gases to stable carbon and hydrogen oxides (i.e., CO₂ and H₂O) and possibly acid gases (e.g., HCl, HF, H₂SO₄, etc). The combustion products are led from combustion furnace 60 through one or more condensers, filters, or scrubbers 80 and 90 that remove unwanted combustion products from the emerging gas stream, or effluent, leaving, in essence, only the inert purge gas and unreacted oxygen in

the resulting stream. In one embodiment of the invention, the combustion products enter Drierite™ adsorbent tube 80 that removes H₂O from the combustion products, and then through Ascarite™ adsorbent tube 90 that removes CO₂ and acid gases from the combustion products. Each of these scrubbers, 80 and 90, are about 6 inches long. Mass flow meter 100 is positioned in the gas flow to measure the mass flow rate of the remaining N₂ and O₂. The oxygen consumed from the gas stream by the oxidation (combustion) reactions is measured at an oxygen analyzer 110 located downstream from the scrubbers 80 and 90. The heat given off by oxidation/combustion of the gases is related to the oxygen consumed in the reactions by an empirical relationship that is well known in the art. Because oxygen analyzer 110 is located downstream from the sample, intermingling, mixing, and diffusion of the combustion gases, nitrogen carrier gas, and remaining oxygen occurs as the flow stream moves through the furnace and scrubbers to the oxygen analyzer. This journey causes the oxygen-time signal to be distorted or "smeared" with respect to the heat release rate of the sample. By minimizing the volume of pyrolysis tube 20, this smearing can be reduced. This desired flow through the calorimeter can be designated "plug flow" where the gases that emerge from the pyrolyzer enter the combustion furnace in the order in which they were produced by the thermally decomposing sample. The fuel gases are arranged from leading edge to trailing edge in a substantially linear distribution, essentially synchronized with the mass loss rate of the sample, according to the order and time when they were liberated in pyrolysis. The present invention maintains substantial plug flow of the fuel and subsequent combustion gases through the combustion calorimeter such that every element of the fuel and subsequent combustion gases has exactly the same residence time in the calorimeter. Consequently, the oxygen consumption pulse shape closely approximates the heat release rate pulse shape of the sample. Since the oxygen consumption pulse is now only slightly distorted with respect to the heat release rate of the sample, standard mathematical transforms can be used to reconstruct the heat release rate pulse from the oxygen consumption-time data. Such mathematical transforms are well-known in the art.

The mathematical transform function that eliminates the distortion in the oxygen consumption pulse shape may be integrated into the oxygen analyzer 110 to directly yield the heat release rate from the oxygen consumption pulse.

I claim:

1. A heat release rate calorimeter providing a quantitative measure of combustion dynamics of a sample comprising:
 - a. means for thermally decomposing said sample under anaerobic conditions to produce fuel gases;
 - b. a furnace for combusting said fuel gases;
 - c. a stream of inert gas for transporting said fuel gases to said furnace in the order in which said fuel gases were produced by said thermally decomposing sample;
 - d. a tube for conducting said fuel gases from said thermal decomposing means to said furnace, said tube confining said gas stream and said fuel gases in substantial plug flow;
 - e. means for inserting a measured amount of oxygen into said inert gas stream and said fuel gases prior to combustion in said furnace;
 - f. means for collecting the gaseous effluent from said furnace;
 - g. means for measuring the amount of oxygen present per unit time in said effluent; and,

- h. means for applying a mathematical transform to compute the heat release rate of said sample from said measured amount of oxygen inserted into said fuel gases and inert gas stream and the measurement of the amount of oxygen present per unit time in said effluent. 5
- 2. A flow calorimeter for measuring the heat release rate of a sample in the milligram range comprising:
 - a. A pyrolysis chamber for thermally decomposing said sample under anaerobic conditions to produce fuel gases; 10
 - b. a furnace for combusting said fuel gases;
 - c. a nitrogen gas stream for transporting said fuel gases to said furnace in the order in which said fuel gases were produced by said thermally decomposing sample; 15
 - d. a narrow tube for conducting said fuel gases to said furnace, said tube confining said nitrogen and said fuel gases in a nitrogen/fuel gas stream in substantial plug flow;
 - e. means for injecting oxygen at a measured rate into said nitrogen/fuel gas stream prior to combustion in said furnace; 20
 - f. means for collecting the gaseous effluent from said furnace after combustion;
 - g. means for removing unwanted substances from said effluent to produce a filtered effluent; 25
 - h. means for measuring the oxygen content of said filtered effluent; and,
 - i. means for applying a mathematical transform to compute the heat release rate of said sample by comparing the amount of oxygen injected into the nitrogen/fuel gas stream prior to combustion with the oxygen content of said filtered effluent. 30
- 3. The calorimeter as in claim 2 wherein the said filtered effluent consists essentially of nitrogen and oxygen. 35
- 4. The calorimeter as in claim 3 wherein said narrow tube has a cross-sectional dimension significantly less than its length.
- 5. A method for providing a quantitative measure of combustion dynamics of a sample, comprising the steps of: 40
 - a. thermally decomposing said sample to fuel gases under anaerobic conditions;
 - b. transporting in an inert gas stream said fuel gases in the order in which said fuel gases were produced by said thermally decomposing sample to a furnace; 45

- c. inserting a measured amount of oxygen into said fuel gases and said inert gas stream prior to combustion in said furnace;
- d. conducting said fuel gases and said inert gas stream to said furnace in a narrow tube that confines said fuel gases and said inert gas stream in plug flow;
- e. combusting said fuel gases in said furnace;
- f. collecting the gaseous effluent from said furnace after combustion;
- g. measuring the amount of oxygen present per unit time in said effluent; and,
- h. computing the heat release rate of said sample from said measured amount of oxygen inserted prior to combustion and the measurement of the amount of oxygen present per unit time in said effluent by applying a mathematical transform.
- 6. A method of measuring the heat release rate of a sample in the milligram range comprising the steps of:
 - a. thermally decomposing said sample under anaerobic conditions in a pyrolysis chamber to produce fuel gases;
 - b. transporting by means of a nitrogen gas stream said fuel gases in the order in which said fuel gases were produced by said thermally decomposing sample to a furnace;
 - c. confining said fuel gases and said nitrogen gas stream from said pyrolysis chamber to said furnace in substantial plug flow within a small volume tube;
 - d. injecting a measured amount of oxygen into said fuel gases and nitrogen gas stream prior to combustion in said furnace;
 - e. combusting said fuel gases in said furnace;
 - f. collecting the gaseous effluent from said furnace after combustion;
 - g. removing unwanted substances from said effluent to produce a filtered effluent consisting essentially of said nitrogen gas stream and oxygen;
 - h. measuring the oxygen content of said filtered effluent; and,
 - i. comparing the said measured amount of oxygen injected prior to combustion with the oxygen content of said filtered effluent to calculate the heat release rate of said sample by applying a mathematical transform.

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